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Spin Sensitivity and Magnetic Response Analysis of Nano-SQUIDs

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Abstract. This paper presents the spin sensitivity and magnetic response analysis of the nano-superconducting-quantum-interference devices (SQUIDs). We employed the computational study to understand the schemes of a nano-SQUID's detection capability according to the device's geometry and fabrication process. We find that the performance of the nano-device increased by decreasing the loop size of the SQUIDs, and it reached the maximum value at the corners of the loop. We then estimated the flux noise S_{Φ} of the SQUIDs in the thermal white noise regime and discussed the field amplification factor around the cross-section area. Furthermore, we fabricated $YBa_2Cu_3O_7$ (YBCO) based nano-SQUIDs with Josephson junctions at MgO biocrystal grain boundaries using the Pulsed Laser Deposition (PLD) and Focused Ion Beam (FIB) technique. By comparison with the estimated devices coincides nicely with our estimation.

Keywords. Josephson junction, nanoSQUIDs, simulation, spin sensitivity, microfluidic technology

1. Introduction

Superconducting quantum interference devices (SQUIDs) with direct current (dc) are promising sub-micrometer dimension devices for probing quantum physical systems [1,2], such as small spin systems[3,4] and high sensitivity magnetometry[5]. High-temperature SQUID does not require expensive cryogenic refrigeration equipment, thus more capable as the building block for modern nanoscale applications [6,7,8,9].

A $YBa_2Cu_3O_7$ (YBCO) dc SQUID constitutes a thin film superconducting loop, and Josephson junctions interrupt the loop. It converts the magnetic flux into current or voltage. When the current is more extensive than the Josephson critical current I_0 , the junction switches to a resistive state, and the device's voltage will no longer remain zero due to the cooper pair-tunneling through the junction, shown in Figure. 1. A SQUID with high sensitivity can detect any form of energy that can convert into magnetic flux

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within the loop of the SQUID. Recently, extremely low spin spectral density within the range of hundred nanometers has been reported[8,9]. The SQUID's sensitivity depends strongly on the device's design[10]. To increase the SQUIDs' detecting performance, the magnetic moment down to a single spin level, optimizing the SQUID's design to fabricate an appropriate SQUID sensor is necessary.

Simulation studies of a magnetic nanoparticle at any generic position above the SQUID loop and the corresponding influence to the magnetic flux were reported recently by Granata[2], Tilbrook[11] and Bouchiat[7]. The spin sensitivity of a SQUID layout is $S_{\mu}^{1/2} = S_{\Phi}^{1/2} / \Phi_{\mu}$ [12], in this function S_{Φ} is the magnetic flux noise and Φ_{μ} is the coupling factor. Given that the level of the inductance of the SQUID *L* is proportional to the magnetic flux noise S_{Φ} , it is necessary for us to reduce the inductance in order to increase the sensitivity [6,13]. In order to decrease the inductance, the dimension of the SQUID loop has to be reduced to submicron size. The details of the magnetic coupling between the SQUID device and the single spin need to be studied to predict the response of the SQUID corresponding to a single spin located at different positions within the device[14]. Moreover, this study can provide more perspectives regarding optimizing the SQUID single spin sensor [15].

This paper reports the detailed evaluation process of the SQUID's sensitivity and response relative to the single spin as a function of position within the SQUID loop. We then fabricated YBCO-based nano-SQUIDs with Josephson junctions at MgO biocrystal grain boundaries using the Pulsed Laser Deposition (PLD) and Focused Ion Beam (FIB) technique [16]. The electrical current, magnetic voltage, and noise are measured under liquid nitrogen temperature in an electrically and magnetically shielded environment to characterize the device's properties.



Figure 1. Schematic of the magnetic field passing through nanoSQUIDs.

2. Methodology

2.1. Spin sensitivity computation

To evaluate the spin sensitivity $S_{\mu}^{1/2}$ of the SQUID device, we need to know the coupling factor Φ_{μ} between the spin and SQUID [17]. Let us consider a single spin

 $(\mu_B = 9.3 \times 10 \exp{-24J/T})$ oriented along the *z*-axis, positioned within a rectangular geometry SQUID whose side length is a and width is b (shown in Figure. 2). The spin located at P(x', y', z'). Because the magnetic flux of the spin in the SQUID loop's direction does not contribute to the magnetic threading of the loop. The surface integral of the magnetic field threading by the magnetic moment μ_B over the loop is equal to the path integral of the potential vector of the spin tracing the loop of the SQUID, shown in Equation (5)



Figure 2. A spin located at a generic position within the SQUID loop.

$$\Phi_{\mu} = \oint \mathbf{A}(\mathbf{r}) \cdot d\mathbf{s} \tag{1}$$

Where $\mathbf{A}(\mathbf{r})$ is the magnetic vector potential. The x and y direction components of the magnetic vector potential at generic position P(x', y', z') along the *z*-axis are [8],

$$A_x = -\frac{\mu_0 \mu_B}{4\pi} \frac{y}{\mathbf{r}^3}$$
$$A_y = \frac{\mu_0 \mu_B}{4\pi} \frac{x}{\mathbf{r}^3}$$
(2)

Where **r** is the distance between the spin and the plan of the SQUID loop, and μ_0 is the magnetic vacuum permeability. The magnetic flux of a spin as a function of its position within the loop is,

$$\Phi_{\mu}(x',y',z') = -\frac{\mu_{0}\mu_{B}}{4\pi} \left(\int_{-\frac{b}{2}}^{\frac{b}{2}} \frac{(a/2-x')}{\mathbf{r}^{3}} dy + \int_{\frac{a}{2}}^{-\frac{a}{2}} \frac{(b/2-y')}{\mathbf{r}^{3}} dx + \int_{\frac{b}{2}}^{-\frac{b}{2}} \frac{(-a/2-x')}{\mathbf{r}^{3}} dy + \int_{-\frac{a}{2}}^{\frac{a}{2}} \frac{(-b/2-y')}{\mathbf{r}^{3}} dx\right)$$
(3)

We further expand the above Equation (Equation 2.1) and revised the Equation as below,

$$\begin{split} \Phi_{\mu}(x',y',z') &= -\frac{\mu_{0}\mu_{B}}{4\pi} (\int_{-\frac{b}{2}}^{\frac{b}{2}} \frac{\frac{a}{2}-x'}{[((a/2-x')')^{2}+(y-y')^{2}+z'^{2}]^{3/2}} dy \\ &+ \int_{\frac{a}{2}}^{-\frac{a}{2}} \frac{\frac{b}{2}-y'}{[((x-x')')^{2}+(b/2-y')^{2}+z'^{2}]^{3/2}} dx \\ &+ \int_{\frac{b}{2}}^{-\frac{b}{2}} \frac{-\frac{a}{2}-x'}{[((-a/2-x')')^{2}+(y-y')^{2}+z'^{2}]^{3/2}} dy \\ &+ \int_{-\frac{a}{2}}^{\frac{a}{2}} \frac{-\frac{b}{2}-y'}{[((x-x')')^{2}+(-b/2-y')^{2}+z'^{2}]^{3/2}} dx \end{split}$$
(4)

2.2. Magnetic flux noise

The other most critical factor of a SQUID device is the magnetic flux noise. We use the theoretical expression from Langevin simulations to determine the flux noise of the SQUID in the thermal white noise regime [18,19,20,21],

$$S_{\Phi} = f(\beta_L) \Phi_0 k_B T L / I_0 R \tag{5}$$

Here, the β_L is the screening parameter, I_0 is the critical current, and L is the inductance. For lower values of β_L , S_{Φ} increases. Furthermore, it is important to notice from this Equation that $S_{\Phi} \propto L$. The decreasing inductance will reduce the flux noise. We know that L will decrease with the contribution of miniaturization of the SQUID loop size and increase the thickness of the *YBCO* superconducting film, which means S_{Φ} is linearly dependent on the side length and film thickness of the SQUID.

2.3. Field amplification factor around the cross-section area

In this section, we discuss the magnetic amplification effect around the SQUID loop's cross-section area (constriction or junctions). The layout of the nanoSQUID (top view) is shown in Figure. 3(a). As shown in Figure. 3 (b), *a* and *b* are the width and thickness of the cross-section, respectively, *d* is the length of the constriction, λ is the London penetration depth, *x* and *y* are the widths, and the thickness direction of the cross-section, and z is the length direction of the cross-section [8,4]. Magnetic flux density at the *x* direction over the cross-section with a rectangular cross-section can be calculated using the Biot–Savart law.

$$B_{x}(x',y',z') = -\frac{\mu_{0}}{4\pi} \int_{0}^{b} \int_{0}^{a} \int_{-d/2}^{d/2} \frac{(y'-y)j(x)}{\mathbf{r}^{3}} dx dy dz$$
(6)

Where j(x) he distribution of shielding current, $j(x,y) = j(x) = \frac{1}{2\lambda b}e^{(|x|-a)/\lambda}$.



Figure 3. (a) Schematic diagram of magnetic nanoparticles on top of the cross-section area of a nanoSQUID. (b) Schematic diagram of the structure and coordinate systems of the cross-section area.

3. Results

Solving the analytically expressed Equation (2.1) numerically, we obtained the magnetic flux produced by a single spin as a function of its position within the SQUID loop. Figure. 4 reports the magnetic flux distribution of a single spin at the *xy*-plane, 10*nm* above the SQUID loop. The side length of the SQUID loop is a = 380 nm and b = 220. The highest values of the magnetic flux are obtained when the spin is close to the corner of the loop, as is shown in Figure. 4,.



Figure 4. Distribution of the magnetic flux produced by a single spin within the SQUID loop. The side length of the loop is a = 380nm and b = 220nm. The distance of between the spin and loop's xy-plane is z' = 10nm.

By modifying the distance z' value between the spin and the *xy*-plane of the SQUID loop, we find the dependence in the Equation within $-100nm \le z \le 100nm$ with abso-



Figure 5. Calculating the coupling factor in the range of $-100nm \le z \le 100nm$.

lute values scaling like $\Phi_{\mu} \propto z^{-3/2}$, shown in Figure. 5. Decreasing z direction distance towards the SQUID loop, the values of the magnetic flux increase.

Figure. 6 (a) and (b) show the amplification factor variant along the *x*-direction. By reducing the width of the cross-section from 50nm to 10nm, the maximum amplification factor continuously increases. However, when the width of the cross-section area decreased, the peak of the amplification factor gradually transformed from two peaks on both sides to one peak at the center of the cross-section area. Meanwhile, the peak value of the amplification factor becomes larger. This result indicates that, in order to enhance the sensitivity of the nano-SQUID devices, the particle under test should be positioned above the center of the cross-section of the SQUID loop.



Figure 6. Field amplification factor distribution along the width direction of the cross-section. The distance above the SQUID's loop is 50 nm. (a) a = 50nm. (b) a = 10nm

YBCO films on MgO bicrystal substrates with a 24-degree misorientation angle. We use photolithography to define coarse structures, followed by Ar ion milling. Subsequently, FIB with 30 keV Ga ions in a dual beam Focused Ion Beam (FIB) system patterned the selected bridges into nanoSQUIDs[20,22,23]. We obtained a SQUID device with a 220 nm × 380 nm hole. Figure. 7 presents an SEM image of a YBCO nanoSQUID on a MgO bicrystal. Slightly enhanced white noise level down to $S_{\phi}^{1/2} = 175n\Phi_0/\sqrt{Hz}$ [16], we have made an improvement of the sensitivity of this nano-SQUID devices down to the level of single spin sensitivity, which agrees well with our simulation result.



Figure 7. SEM image of a YBCO nanoSQUID on a MgO bicrystal substrate.

4. Conclusion

We illustrated the schemes of a nano-SQUID's detection capability according to the device's geometry and fabrication process. We demonstrated that the performance of the nano-device increased by decreasing the loop size of the SQUIDs, and it reached the maximum value at the corners of the loop. We estimated the flux noise S_{Φ} of the SQUIDs in the thermal white noise regime and found S_{Φ} is linearly dependent on the side length and film thickness of the nano-SQUID. We found that the field amplification factor around the cross-section area increases when shrinking the width of the cross-section area of the SQUID loop. We have successfully produced the YBCO-based nano-SQUIDs with Josephson junctions at MgO biocrystal grain boundaries. The spin sensitivity evaluated by the experimentally fabricated devices is comparable with our estimation.

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