

Research on Optimization Method of Tool Path in Five-Axis Process Singular Region

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Abstract. For the five -axis machine into the singular region in the process of parts processing, resulting in a discontinuous and rapid rotation of the axis of rotation of large angles. Based on the analysis of the cause of the obvious ripple on the machined surface and the influence on the machining precision, a mathematical model of the singular region is established, and an optimization method of the tool path in the singular region is proposed. The simulation and practical machining results show that the method can effectively overcome the problem of excessive movement of the rotating shaft in the Song singular region of 5-axis machine tool, and solve the surface corrugated defects caused by the problem, while improving the processing efficiency.

Keywords. Digital control process, Singular region, Tool path optimization

1. Introduction

The shape of aircraft structural parts is related to the aerodynamic layout of the aircraft, and the machining quality of the shape is closely related to the aerodynamic performance. Therefore, most of the contour surfaces of aircraft structural parts are curved, which need five -axis NC machine tools to complete.

The five-axis machining adds two rotating shafts to the three-axis machining, which makes the machining mode more flexible, the material removal rate is higher, the processing time is shorter, and the more complex parts can be dealt with. Therefore, five-axis machining has been widely used in aviation, aerospace, automobile, ship and other industrial fields. But the motion of rotation axis also makes the attitude control of tool more complex, which introduces many special problems of five axis machining. The singular point problem is an important one. When the tool passes through the region near the singular point, the rotation axis will produce discontinuous and rapid rotation, which greatly increases the non-linear error, and it is easy to destroy the workpiece, and even damage the machine parts.

Because of the existence of singular region, when the five -axis NC machining is carried out, it is easy to appear in a very short cutting length, the rotating axis rotates rapidly and discontinuously, and the variation is very large, which will produce obvious ripples on the machined surface, resulting in a great increase in the amount of grinding and grinding difficulty of the subsequent fitters, which seriously affects the

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machining quality of the parts and reduces the machining efficiency of the parts [1], as shown in Figure 1.

Therefore, it is very important to optimize the tool path in the singular region for improving the machining accuracy and efficiency [2]. In this paper, the cutter axis vector in the singular region is taken as the research object to solve the problem that the motion of rotation axis in the singular region is too large. In order to improve the machining accuracy and efficiency of five axis machine tool, the relevant research is carried out by means of theoretical analysis, mathematical calculation, computer programming and experimental verification. Finally, the tool path optimization software is formed, and the optimization method is verified by simulation analysis and trial cutting. The processing quality and efficiency are improved synchronously.

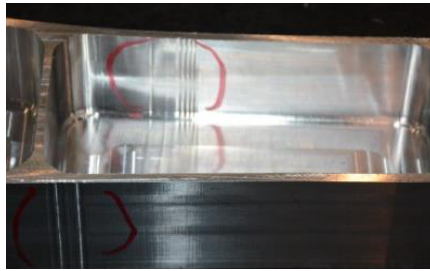


Figure 1. Surface ripple caused by excessive movement of the axis of rotation.

2. Theoretical study on the optimization method of tool path in singular region

Singular region is characterized by very large changes in the axis of rotation when the tool-axis vector changes very little one-dimensional angle [3]. Therefore, through the establishment of singular region tool path optimization mathematical model, analysis of the surface profile error as a guide to calculate the tool axis variation tolerance, The optimization vector is found in the tolerance region to minimize the angle between the starting vector and the target vector on the projection plane, so that the motion of the rotation axis in the singular region is minimized.

2.1. Singularities in 5 Axis Machine Tools

In 5-axis NC machining the so-called singular problem arises when there is inverse kinematics singular point in the machining space [4]. The inverse kinematics problem of machine tool can be expressed as solving the coordinates of each moving axis of the machine tool under the condition of known coordinate value of tool tip in workpiece coordinate system and vector direction of cutter axis. Take the AC double turntable five-axis machine tool as an example. The solution of A and C angles is obtained from the inverse kinematic transformation as follows [5]:

$$\begin{cases} A = k_A \cdot \alpha \cos(k) & k_A = \pm 1 \\ C = -\arctan\left(\frac{i}{j}\right) + k_C \cdot \pi, & k_C = 0,1,2 \end{cases} \quad (1)$$

where i, j, k is tool vector, A is in $[-90^\circ, 90^\circ]$, C is in $[0^\circ, 360^\circ]$. The value of A, C in Table 1 and Table 2 based on Eq. (1).

Table 1. AC corner numerical value($A \in [-90^\circ, 0^\circ]$).

$A \in [-90^\circ, 0^\circ]$	i	>0	<0	<0	>0	$=0$
	j	>0	>0	<0	<0	>0
	C	$2\pi - \arctan(i/j)$	$-\arctan(i/j)$	$\pi - \arctan(i/j)$	$\pi - \arctan(i/j)$	2π
	i	$=0$	>0	<0	$=0$	
	j	<0	$=0$	$=0$	$=0$	
	C	π	$3\pi/2$	$\pi/2$	Can't be sure.	

Table 2. AC corner numerical value($A \in (0^\circ, 90^\circ]$).

$A \in (0^\circ, 90^\circ]$	i	>0	<0	<0	>0	$=0$
	j	>0	>0	<0	<0	>0
	C	$\pi/2 - \arctan(i/j)$	$\pi - \arctan(i/j)$	$2\pi - \arctan(i/j)$	$-\arctan(i/j)$	π
	i	$=0$	>0	<0	$=0$	
	j	<0	$=0$	$=0$	$=0$	
	C	2π	$\pi/2$	$3\pi/2$	Can't be sure.	

From the Table 1, it can be seen that there is no singular problem in the solution of angle A , but when the solution of angle c is in $i=0$ and $j=0$, the solution of $c = \pi - \arctan(0/0)$ or $C = -\arctan(0/0)$ has no solution, so it is impossible to determine the value of c , that is to say, it is singular point. At this time, the turntable of the machine tool and the tool shaft are vertical, no matter what the value of the C angle does not affect the direction of the tool axis of the point, that is, the c axis can swing at any angle to obtain the tool axis vector at the singular point position, so for the AC double turntable five-axis machine, the point of the tool axis vector is the singularity point, and the normal axis of the C turntable is the singular axis.

In fact, When the angle between the tool axis vector and the singular axis is less than a certain angle, the angle of the rotation axis will change more and more, resulting in large error [6]. This angle is singular value, and the area formed by it is a cone area in space, as shown in the Figure 2.

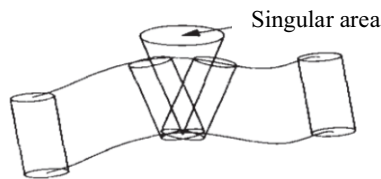


Figure 2. Schematic diagram of singular regions.

2.2. Mathematical Modeling of Singular Regions

According to the definition of singular region, the geometric model of the singular region is established, as shown in Figure 3.

In Figure 3, V_1 and V_2 represent the starting vector and target vector of tool axis motion, respectively, the angle between the starting vector and the target vector on the

projection plane, O for the origin, V_p for the polar axis, V_p as the axis, V_1 and V_2 vectors as the busbar as the conical surface, and projection to the plane as circle A.

When the angle between V_1 , V_2 and polar axis V_p is very small, even if the angle between V_1 and V_2 is very small, But the angle $\Delta\beta$ of their projection on the plane of the polar axis V_p as the normal vector may be very large. This is the reason why the tool axis vector on the same surface changes very little, but the machine tool rotation axis movement still needs to swing substantially.

Secondly, after understanding the problems existing in the singular region, in order to reduce the movement of the rotation axis, the tool path in the singular region must be optimized. The optimization principle is to establish the mathematical model of the tool path optimization, as shown in Figure 4. The results show that the variation tolerance of the tool axis is calculated by using the machining surface profile error as the guide, and the optimal vector is found in the allowable region to minimize the $\Delta\beta$, so as to minimize the movement of the rotation axis in the singular region.

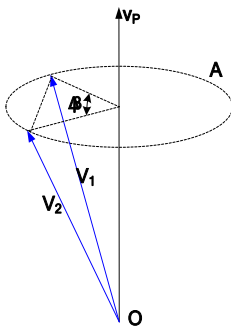


Figure 3. The geometric model of singular region.

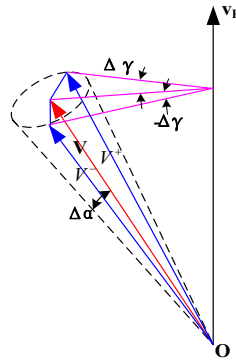


Figure 4. Geometric model of tool path optimization.

In Figure 4, the vector V to be optimized is used as the center line of rotation, the origin O is taken as the item point, and the tolerance $\Delta\alpha$ as the half-top angle as the conical face. The angles between the bus and the vector V of the conical surface is $\Delta\alpha$. The super polar axis V_p does two planes tangent to the conical surface, and the tangent vectors are represented by vectors V^- and V^+ .

The projection angles of V^- and V^+ on the plane where the polar V_p is the normal vector are $\Delta\gamma$ and $-\Delta\gamma$, respectively. V and V^- , V^+ make plane p' and p'' respectively. The previous tool axis vector is used as the optimization objective vector of the current tool axis, and the included angle θ of the projection between the optimization objective vector and the vector V_{TARGET} to be optimized on the plane where the polar axis V_p is the normal vector is calculated.

Assuming that V is the vector optimized by the cutter axis, it can be divided into four cases by geometric judgment

Case 1: $\theta < -\Delta\gamma$ is $V_y = V^-$;

Case 2: $\theta > \Delta\gamma$ is $V_y = V^+$;

Case 3: $0 < \theta < \Delta\gamma$, V_y is p'' with the intersection of the target vector V_{TARGET} and the plane of the polar axis.

Case 4: $-\Delta\gamma < \theta < 0$, V_y is p' with the intersection of the target vector V_{TARGET} and the plane of the polar axis.

2.3. Tool Path Optimization Method

Generally, the motion path of five axis CNC machine tool (tool path) is obtained by CAM software, and the running NC program can be recognized by post-processing software. We can optimize the tool path through post-processing software to solve the problem of singular region. According to the mathematical model of tool path optimization in singular region, the flow diagram of tool path optimization is shown in Figure 5.

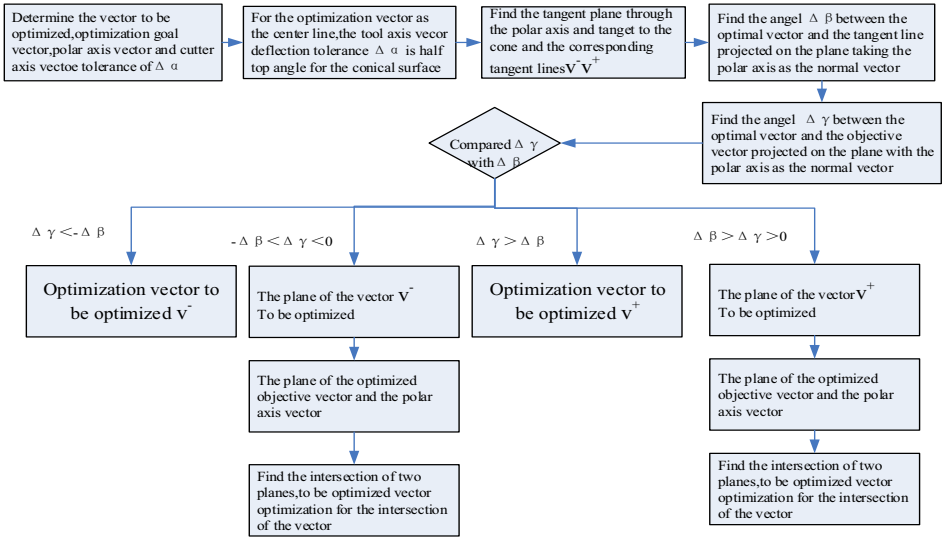


Figure 5. the flow diagram of tool path optimization.

Know: Optimize tool vector $v_1 = (i_1 \ j_1 \ k_1)$, optimizing vector $v = (i \ j \ k)$, axis vector $v_p = (i_p \ j_p \ k_p)$, tolerance $\Delta\alpha$

Find: Optimize the cutter axis vector $v_y = (i' \ j' \ k')$, make the angle between the tool axis vector and the vector to be optimized $(v_p \ v) < \Delta\alpha$, and projected on the plane with the polar vector as the normal vector of the objective optimization vector $|\text{Ang}(v_y \ v_1 \ v_p)|$.

By the above analysis, the model can be reduced to a three-dimensional quadratic system of equations.

$$\left\{ \begin{array}{l} \begin{pmatrix} i \\ j \\ k \end{pmatrix} \bullet \begin{pmatrix} i' \\ j' \\ k' \end{pmatrix} = \cos \alpha \\ \left(\begin{pmatrix} i \\ j \\ k \end{pmatrix} \times \begin{pmatrix} i' \\ j' \\ k' \end{pmatrix} \right) \bullet \left(\begin{pmatrix} i_p \\ j_p \\ k_p \end{pmatrix} \times \begin{pmatrix} i'_p \\ j'_p \\ k'_p \end{pmatrix} \right) = 0 \\ \left\| \begin{pmatrix} i' \\ j' \\ k' \end{pmatrix} \right\| = 1 \end{array} \right. \quad (2)$$

Put Eq. (2) simplify

$$\left\{ \begin{array}{l} ii' + jj' + kk' = \cos \alpha \\ (jk' - kj')i_p + (ki' - ik')j_p + (ij' - ji')k_p = 0 \\ i'^2 + j'^2 + k'^2 = 1 \end{array} \right. \quad (3)$$

From the Eq. (3) the optimized polar axis of the cutter axis vector can be obtained by the mathematical calculation $v_y = (i' \ j' \ k')$.

3. Software Development and Software Testing of Tool Path Optimization in Singular Region

In order to realize the automatic optimization of tool path, reduce the difficulty of calculation, improve the working efficiency, and facilitate the engineering application, this paper develops the tool path optimization processing software based on VB.NET language, and verifies that the function of the software meets the requirements of tool path optimization by optimizing the preprogram of typical parts.

3.1. Software Development

The software input is the tool path file processed by CAM. The tool axis vector in the file is identified line by line, and the tool axis vector (target vector) meeting the optimization conditions is identified as 0. Then read the tool axis vector marked as 0 for optimization. The tool axis vector after optimization is judged. If the tool axis vector meets the requirements of optimization objectives, the tool axis vector is identified as 1. If it does not meet the requirements of optimization objectives, the optimization cycle will be carried out until the requirements of optimization objectives are met. The software running framework is shown in the Figure 6.

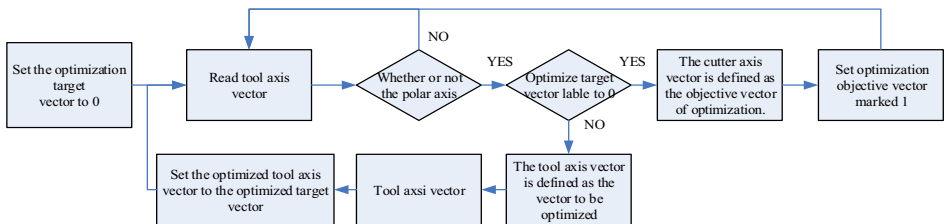


Figure 6. Block diagram of software.

3.2. Software Testing

After the completion of the software, the ability test is carried out to test whether the software can effectively optimize the cutter axis vector, reduce the amount of rotation axis movement, and realize the tool of tool-path optimization method.

The "S" specimen is taken as the specimen for testing the machining accuracy of the machine tool in five axes. Its structure is shown in Figure 7. In the label area, there is a typical singular region problem, so we choose "S" pre-program to optimize the test.

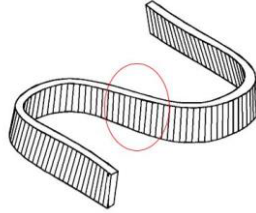


Figure 7. The schematic diagram of "S" specimen.

NC program of singular region before and after optimization are shown in Figure 8. Before the optimization, C angle enters and leaves from the singular region of s specimen, and then decreases from 113° to -34° . The C angle is transported in a short time. After optimization, the C angle remained almost unchanged at -230° , effectively reducing the C angle movement.

N1011 X0.335 Y38.697 Z30.256 A-6.995 C-229.351	N1011 X0.482 Y38.382 Z30.211 A-6.709 C113.982
N1012 X0.865 Y37.351 Z30.227 A-6.794 C-229.654	N1012 X1.009 Y37.034 Z30.182 A-6.509 C113.174
N1013 X1.432 Y35.871 Z30.194 A-6.565 C-229.935	N1013 X1.574 Y35.553 Z30.149 A-6.283 C112.278
N1014 X1.954 Y34.477 Z30.161 A-6.345 C-230.162	N1014 X2.092 Y34.158 Z30.117 A-6.064 C111.420
N1015 X2.599 Y32.701 Z30.118 A-6.055 C-230.378	N1015 X2.734 Y32.381 Z30.075 A-5.779 C110.296
N1016 X3.209 Y30.977 Z30.075 A-5.766 C-230.517	N1016 X3.341 Y30.655 Z30.032 A-5.497 C109.159
N1017 X3.783 Y29.311 Z30.031 A-5.479 C-230.582	N1017 X3.913 Y28.988 Z29.990 A-5.217 C107.998
N1018 X4.288 Y27.811 Z29.991 A-5.218 C-230.585	N1018 X4.416 Y27.487 Z29.951 A-4.962 C106.887
N1019 X4.847 Y26.116 Z29.944 A-4.913	N1019 X4.973 Y25.793 Z29.906 A-4.670 C105.535
N1020 X5.399 Y24.691 Z29.904 A-4.653	N1020 X5.432 Y24.368 Z29.867 A-4.422 C104.297
N1021 X5.864 Y22.947 Z29.852 A-4.327	N1021 X5.983 Y22.627 Z29.819 A-4.117 C102.625
N1022 X6.409 Y21.200 Z29.799 A-3.995	N1022 X6.525 Y20.883 Z29.770 A-3.810 C100.729
N1023 X6.940 Y19.470 Z29.744 A-3.659	N1023 X7.053 Y19.157 Z29.720 A-3.506 C98.567
N1024 X7.435 Y17.836 Z29.691 A-3.338	N1024 X7.545 Y17.527 Z29.672 A-3.221 C96.188
N1025 X7.890 Y16.315 Z29.640 A-3.036	N1025 X7.997 Y16.011 Z29.627 A-2.959 C93.592
N1026 X8.379 Y14.664 Z29.582 A-2.704	N1026 X8.482 Y14.367 Z29.578 A-2.679 C90.234
N1027 X8.799 Y13.232 Z29.530 A-2.415	N1027 X8.899 Y12.940 Z29.535 A-2.445 C86.727
N1028 X9.301 Y11.504 Z29.465 A-2.063	N1028 X9.397 Y11.220 Z29.483 A-2.174 C81.536
N1029 X9.801 Y9.771 Z29.396 A-1.707	N1029 X9.894 Y9.494 Z29.430 A-1.923 C74.929
N1030 X10.290 Y8.063 Z29.323 A-1.355	N1030 X10.380 Y7.794 Z29.378 A-1.707 C66.650
N1031 X10.783 Y6.338 Z29.242 A-0.998	N1031 X10.870 Y6.077 Z29.327 A-1.533 C56.166
N1032 X11.305 Y4.501 Z29.146 A-0.618	N1032 X11.389 Y4.250 Z29.273 A-1.420 C42.715
N1033 X11.850 Y2.580 Z29.033 A-0.220	N1033 X11.931 Y2.339 Z29.218 A-1.394 C27.216
N1034 X12.394 Y0.760 Z28.937 A0.000	N1034 X12.451 Y0.511 Z29.167 A-1.463 C12.928
N1035 X12.933 Y-1.141 Z28.924 A0.401	N1035 X12.990 Y-1.378 Z29.116 A-1.619 C0.320
N1036 X13.457 Y-2.977 Z28.903 A0.782	N1036 X13.513 Y-3.204 Z29.068 A-1.830 C-9.301
N1037 X13.997 Y-4.854 Z28.875 A1.168	N1037 X14.051 Y-5.071 Z29.019 A-2.085 C-16.827
N1038 X14.528 Y-6.687 Z28.843 A1.542	N1038 X14.582 Y-6.895 Z28.972 A-2.361 C-22.425
N1039 X15.071 Y-8.538 Z28.809 A1.914	N1039 X15.123 Y-8.737 Z28.926 A-2.654 C-26.760
N1040 X15.598 Y-10.377 Z28.790 A2.386	N1040 X15.664 Y-10.556 Z28.880 A-2.954 C-30.080
N1041 X16.147 Y-12.200 Z28.753 A2.746	N1041 X16.213 Y-12.372 Z28.834 A-3.258 C-32.677
N1042 X16.701 Y-14.010 Z28.714 A3.088	N1042 X16.766 Y-14.176 Z28.789 A-3.561 C-34.715
N1043 X17.263 Y-15.809 Z28.674 A3.419	N1043 X17.327 Y-15.971 Z28.744 A-3.863 C-36.319
N1044 X17.832 Y-17.597 Z28.634 A3.740	N1044 X17.896 Y-17.755 Z28.701 A-4.160 C-37.576
N1045 X18.409 Y-19.372 Z28.595 A4.051	N1045 X18.474 Y-19.528 Z28.658 A-4.453 C-38.550
N1046 X18.996 Y-21.134 Z28.555 A4.350	N1046 X19.062 Y-21.289 Z28.616 A-4.737 C-39.286
N1047 X19.593 Y-22.881 Z28.515 A4.636	N1047 X19.662 Y-23.036 Z28.575 A-5.014 C-39.817
N1048 X20.202 Y-24.611 Z28.476 A4.909	N1048 X20.273 Y-24.769 Z28.535 A-5.282 C-40.161
N1049 X20.823 Y-26.324 Z28.438 A5.168	N1049 X20.898 Y-26.486 Z28.497 A-5.542 C-40.318

Pre-optimization

Optimization

Figure 8. Comparison of Pre-optimization program and Optimization program.

Statistical optimization program C Angle travel range and C Angle total movement, the data as shown in Table 3, we can see, the range of C angle travel is -234° to 277° before optimization and -230° to -82° after optimization.

Table 3. "S" specimen simulation of the cutting results.

Contrast items.	Before optimization	After optimization
The range of C	-234°~277°	-230°~-82°
C angle exercise	10892.916°	4669.791°

Therefore, after testing, the software can achieve tool path optimization algorithm, to reduce the rotation axis of the target to be.

4. Application and Verification of Tool-Path Optimization Method in Singular Region

The tool path optimization software is used to optimize the typical parts. Through simulation analysis and trial cutting, the machining states of the parts before and after optimization are compared to verify the optimization effect of the tool path optimization method in the singular region.

4.1. Tool Path Optimization Simulation Analysis

Select a typical part of the tool path optimization test verification, the simulation diagram of trial cutting part model formed by Vericut (A simulation software for NC machining) as shown in Figure 9.

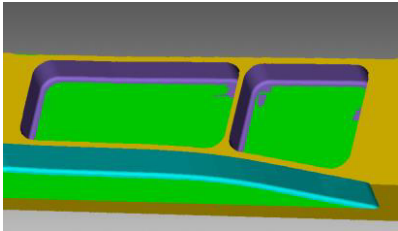


Figure 9. Simulation diagram of trial cutting part model.

The part outline program is optimized before and after the comparison, as shown in Figure 10. The tool path file processed by CAM was imported into the software for optimization. The N2172-N2185, a typical C angle with a large variation, is selected for case study.

2176 N2170 X169.336 Y41.895 Z-12.524 A3.838	2176 N2171 X169.099 Y37.287 Z-12.600 A3.237 C-182.881
2176 N2171 X169.104 Y37.287 Z-12.600 A3.237 C-181.287	2177 N2172 X168.748 Y30.311 Z-12.714 A2.323 C-182.881
2177 N2172 X168.751 Y30.311 Z-12.714 A2.323 C-181.287	2178 N2173 X168.395 Y23.294 Z-12.828 A1.401 C-182.881
2178 N2173 X168.397 Y23.294 Z-12.828 A1.401 C-181.287	2179 N2174 X168.031 Y16.061 Z-12.945 A0.451 C-182.879
2179 N2174 X168.031 Y16.061 Z-12.945 A0.451 C-181.287	2180 N2175 X168.032 Y15.638 Z-12.952 A0.405 C-172.340
2180 N2175 X168.028 Y15.637 Z-12.952 A0.405 C-181.287	2181 N2176 X168.114 Y15.223 Z-12.959 A0.362 C-187.525
2181 N2176 X168.106 Y15.221 Z-12.959 A0.362 C-181.287	2182 N2177 X168.300 Y14.843 Z-12.967 A0.314 C-155.663
2182 N2177 X168.292 Y14.842 Z-12.967 A0.314 C-181.287	2183 N2178 X168.566 Y14.515 Z-12.975 A0.281 C-161.654
2183 N2178 X168.561 Y14.514 Z-12.975 A0.281	2184 N2179 X168.885 Y14.237 Z-12.982 A0.229 C-160.292
2184 N2179 X168.881 Y14.236 Z-12.982 A0.229 C-181.287	2185 N2180 X169.243 Y14.010 Z-12.988 A0.115 C-133.171
2185 N2180 X169.243 Y14.010 Z-12.988 A0.000	2186 N2181 X169.637 Y13.854 Z-12.993 C-53.396
2186 N2181 X169.637 Y13.854 Z-12.993	2187 N2182 X170.057 Y13.801 Z-12.997 A0.162 C-20.737
2187 N2182 X170.054 Y13.801 Z-12.997 A-0.162 C-181.286	2188 N2183 X170.473 Y13.870 Z-12.999 A0.081 C-13.773
2188 N2183 X170.474 Y13.870 Z-12.999 A0.000	2189 N2184 X170.867 Y14.027 Z-13.000 A0.001 C0.000
2189 N2184 X170.867 Y14.027 Z-13.000	2190 N2185 X176.164 Y16.433 Z-13.000 A0.000 C-63.435
2190 N2185 X176.164 Y16.433	2191 N2186 X181.635 Y18.817
2191 N2186 X181.635 Y18.817	2192 N2187 X186.339 Y20.794
2192 N2187 X186.339 Y20.794	2193 N2188 X191.062 Y22.710
2193 N2188 X191.062 Y22.710	2194 N2189 X195.814 Y24.569
2194 N2189 X195.814 Y24.569	2195 N2190 X200.603 Y26.374
2195 N2190 X200.603 Y26.374	2196 N2191 X205.429 Y28.125
2196 N2191 X205.429 Y28.125	2197 N2192 X210.294 Y29.822

postoptimality before optimization

Figure 10. Comparison of actual optimization.

Before optimization, the C angle of the program changes rapidly from -182.8°to C0°. After optimization, the range of C angle variation is very small, and there is no

change at all. Therefore, the optimization of C angle variation in the optimization process is basically the same as that in C -63.4. The effect is obvious as shown in Figure 11.

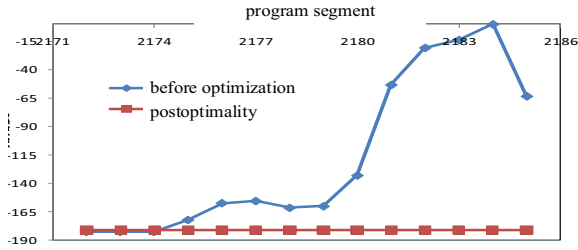


Figure 11. C angle change before and after optimization.

4.2. Verification and Application of Cutter Path Optimization Test

In order to verify the effectiveness of the tool path optimization method, some typical parts are tested and verified on the spot. The real-time machining time of the pre optimization and post optimization of the inner contour of the test cutting part is accurately collected by the DNC real-time monitoring module of the machine tool. The specific values are shown in Table 4.

Table 4. Comparison of actual cutting time before and after optimization.

	pre-process work time	after optimization work time	Shorten processing time	Improve processing efficiency
Contour finishing process	270s	187s	83s	44.38%
Inner form finishing process	221s	123s	98s	79.67%

As can be seen from Table 4, the processing time before shaper optimization is 270s. After optimization, the efficiency is 44.38%, the pre-process time is 221s, after optimization 123s, improve processing efficiency is 79.67%.

The actual cutting effect is shown in Figure 12, 13 and 14. Before the optimization of the surface of the surface are corrugated, seriously affecting the surface quality, the need for benchwork follow-up grinding, but also for the final delivery of parts of the quality of filling the hidden dangers.



Figure 12. Comparison before and after optimization.

After the optimization, the surface waviness has disappeared completely. The effect is good. Not only the machining efficiency is improved, but also the surface quality is greatly improved. It is verified that the optimization method of tool path in singular region can effectively solve the problem of workpiece surface waviness caused by oversized rotation axis of machine tool, and improve machining efficiency at the same time.



Figure 13. Surface Before Optimization

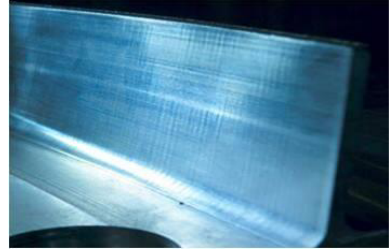


Figure 14. Surface After Optimization

5. Conclusions and Prospects

Based on this method, the tool path optimization software of singular region is developed. Through the simulation comparison and trial test, it is verified that this method can effectively solve the problem of workpiece surface waviness caused by the excessive rotation axis of the machine tool, and can also improve the machining efficiency significantly.

Looking ahead, as the new research project cycle is getting shorter and shorter, aircraft junction component quality requirements are getting higher and higher, five-axis NC machining applications will also be more and more. The engineering application and popularization of tool path optimization software can effectively improve the quality and efficiency of zero-part machining, so as to alleviate the pressure of production delivery and quality. We will continue to study the tool path optimization of five-axis machine tool in the future to make the tool path optimization method more reasonable and more effective, while optimizing and promoting tools software, strengthen engineering application, solve practical problems in production.

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